

TANK GEOMETRY

Tank Internal Diameter	D	=	3000	mm
Height of the Tank	H	=	3600	mm
Tank Shell thickness	ts	=	8	mm
Tank Base thickness	tb	=	8	mm

FOUNDATION GEOMETRY

Width of the Ringwall	w	=	0.650	m
Height of the Ringwall above HPP	h ₁	=	1000	mm
Depth of the Ringwall below HPP	h ₂	=	1000	mm
Width of foundation ring ,W	W	=	5.5	m
Thickness of slab	tc	=	650	mm

Total height of the Ringwall h = 2000 mm

Inner diameter of the ringwall = 3-0.65 = 2.350 m

Outer diameter of the ringwall = 3+0.65 = 3.650 m

Width of liquid column on the ringwall a = $0.65 \times 1000 / 2 - 8 / 2 = 321.0$ mm

Area of the ring A_r = $\pi \times (3.65^2 - 2.35^2) / 4 = 6.13$ m²

Section modulus of the ring Z_r = $\frac{\pi \times (3.65^4 - 2.35^4)}{(32 \times 3.65)}$

= 3.95 m³

Radius of centre line of ring wall,R = 2.00 m

Inner radius of the ring wall,R_{r1} = 1.35 m

Outer radius of the ring wall,R_{r2} = 2.33 m

Inner radius of the ring wall footing,R_{f1} = 4.50 m

Outer radius of the ring wall footing,R_{f2} = 6.50 m

I_{RING WALL} = $(3.14/64) \times (R_{r2}^4 - R_{r1}^4) = 1.27$ m⁴

Z_{RING WALL} = I_{RING WALL}/R_{r2} = 0.55 m³

I_{RING WALL FOOTING} = $(3.14/64) \times (R_{f2}^4 - R_{f1}^4) = 67.46$ m⁴

Z_{RING WALL FOOTING} = I_{RING WALL FOOTING}/R_{f2} = 10.38 m³

Area of ring wall footing,A_{fr} = $(3.14 \times (6.5^2 - 4.5^2)) = 69.08$ m²

Area of ring wall,A_w = $(3.14 \times (2.325^2 - 1.35^2)) = 11.25$ m²

SOIL DATA

Unit weight of soil Y_{Soil} = 19.00 kN/m³

Unit weight of sand fill Y_F = 19.00 kN/m³ (assumed)

Net SBC of soil at foundation depth = 48.00 kN/m²

Allowable Gross SBC (Without Seismic or wind) = 48 + (1 x 19) = 67.00 kN/m²

Allowable Gross SBC (With Seismic or wind) = (48 x 1.25) + (1 x 19)

Allowable Gross SBC (With Seismic or wind) SBC = 79.00 kN/m²

Angle of Internal friction Ø = 30.00 °

Earth pressure coefficient at rest Ko = 1 - sinØ

= 0.50

LOAD DATA FROM MDS

Empty Weight of the Tank (refer MDS)	EL	=	15.00	T
		=	147.15	kN
Operating volume (working capacity - refer MDS)		=	25.00	m ³
Operating Weight of liquid (refer MDS)		=	245.25	kN
Operating Weight (including empty weight)	OL	=	25.00	T
Operating Weight (including empty weight)	OL	=	245.25	kN
Hydrotest volume (Normal capacity-refer MDS)		=	25.00	m ³
Hydrotest Weight of liquid (Refer MDS)		=	245.25	kN
Hydrotest Weight (including empty weight)	HL	=	25.00	T
Hydrotest Weight (including empty weight)	HL	=	245.25	kN

Loading	Condition	Empty	Operating	Test
Shear force at top of foundation level (kN)	WIND	3.83	3.83	-
	SEISMIC	-	46.54	-
Moment at top of foundation level (kNm)	SEISMIC	-	0.00	-
	WIND	0.00	0.00	-

5.75

Seismic Load	Shear	SL _F	=	46.54	kN
	Moment	SL _M	=	0.00	kNm
Live load on roof		LL _r	=	1.20	kN/m ²
Total live load on roof		LL	=	$\pi \cdot 3.008^2 / 4 \cdot 1.2$	
			=	8.53	kN

LOADS ON FOUNDATION

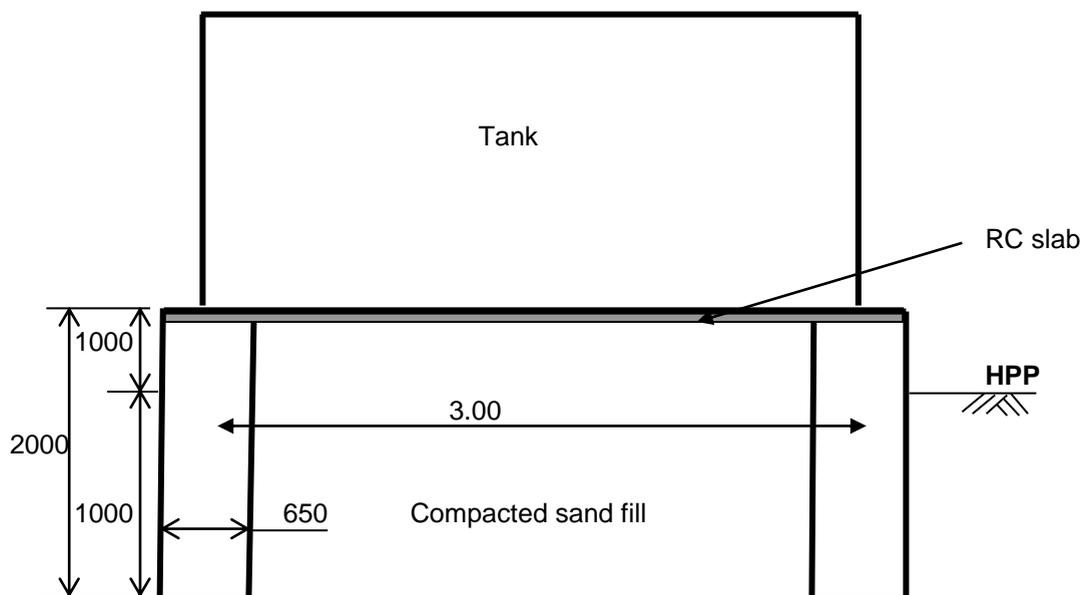
Design Liquid Column = $(25 / (\pi^2 / 4 \cdot 3^2)) \cdot 1000$	H _D	=	3537	mm
Hydrotest Liquid Column (Height of tank)	H _T	=	3600	mm

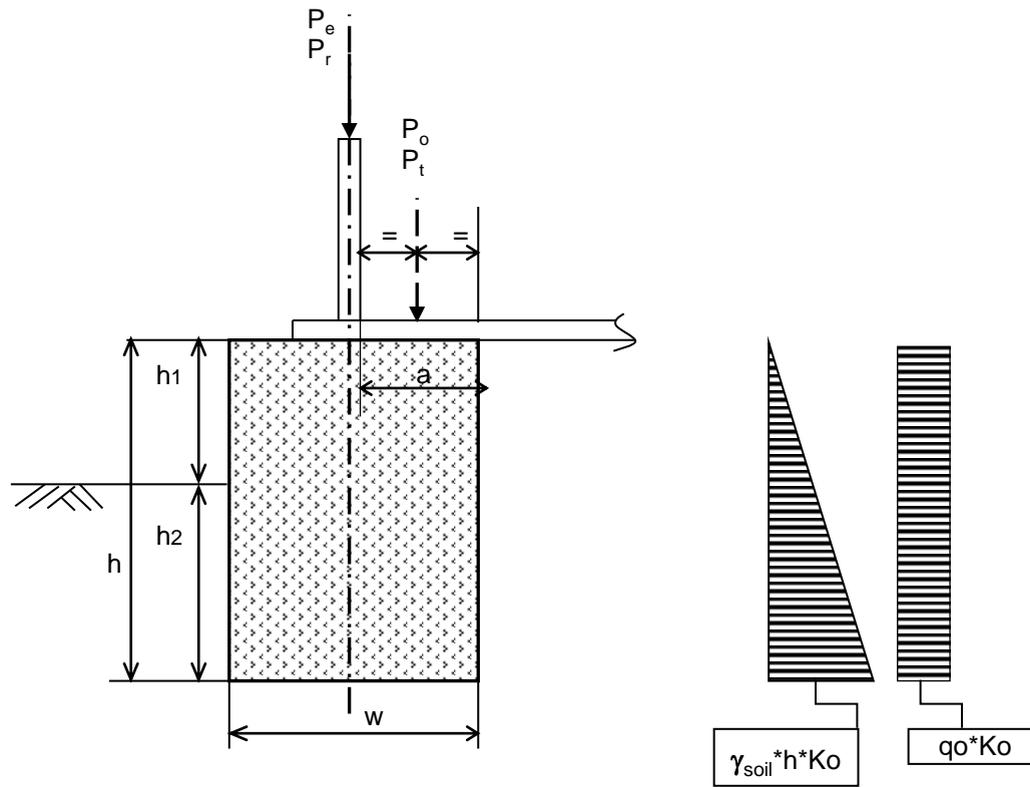
Unit weight of Design Fluid	Y _D	=	10.00	kN/m ³
Unit weight of Test Fluid	Y _T	=	10.00	kN/m ³
Unit weight of concrete	Y _C	=	30.00	kN/m ³
Unit weight of Steel	Y _S	=	78.50	kN/m ³

Load elements directly on the Ringwall

Empty weight of tank on ringwall excluding the base plate

P _e	=	$(147.15 - \pi \cdot 2.35^2 / 4 \cdot 0.008 \cdot 78.5) / (\pi \cdot 3)$
	=	15.32 kN/m
Weight of operating fluid on the ringwall	=	$10 \cdot 3.537 \cdot 0.321$
P _o	=	11.35 kN/m
Weight of test fluid on the ringwall & slab	=	$10 \cdot 3.6 \cdot 0.321$
P _t	=	11.56 kN/m
Load on ringwall due to roof live load	=	$8.528 / (\pi \cdot 3)$
P _r	=	0.90 kN/m





Calculation of Pressure under the Ringwall foundation

Pressure due to the empty weight of tank	EL	=	15.32/69.08	
		=	0.22	kN/m ²
Pressure due to operating fluid	OL	=	11.35/69.08	
		=	0.16	kN/m ²
Pressure due to test fluid	TL	=	11.56/69.08	
		=	0.17	kN/m ²
Pressure due to roof live load	LL	=	0.9/69.08	
		=	0.01	kN/m ²
Pressure due to self weight of the ringwall	DL	=		
		=	36.28	kN/m ²

**STABILITY CHECK
CHECK FOR BEARING PRESSURE**

Load case	LOAD COMBINATION	P/A	M/Z	Pmax	Pmin
1	0.9DL+0.9EL+0.5WL	32.85	0.73	33.58	32.12
2	DL+OL+LL	8.45	0.00	8.45	8.45
3	DL+OL+LL+WL	36.67	1.45	38.12	35.22
4	DL+OL+0.5LL+SL	36.67	23.54	60.21	13.12
5	DL+TL+0.5LL+0.5WL	36.67	0.73	37.40	36.31

CASE 1 : (0.9DL+0.9EL+0.5WL)

Shear force at the base of the tank (due to wind)		=	3.83	kN
Total moment on the ringwall at the base of foundation		=	(5.75)*0.5	
		=	2.88	kNm
Pressure due to Wind load	M/Zr	=	2.88/3.95	
		=	0.73	kN/m ²
Maximum pressure below ring wall		=	0.9* 0.22+0.73+ 0.9* 36.28	
		=	33.58	kN/m ²
			< Net SBC. OK	

Minimum pressure below ring wall = $0.9 \times 0.22 - 0.73 + 0.9 \times 36.28$
= 32.12 kN/m²
No Tension. Hence OK.

CASE II : DL+OL+LL

Pressure below the ringwall = $0.22 + 0.16 + 0.01 + 36.28$
= 8.45 kN/m²
< Net SBC. OK

Pressure below the tank = $0.63 + 35.37 + 25.65 + 19.5$
= 61.65
< Net SBC. OK

CASE III : DL+OL+LL+WL

Shear force at the base of the tank = 3.83 kN

Total moment on the ringwall at the base of foundation = 5.75 kNm

Pressure due to Wind load M/Zr = $5.75 / 3.95$
= 1.45 kN/m²

Maximum pressure below ring wall = $0.22 + 0.16 + 1.45 + 0.01 + 36.28$
= 38.12 kN/m²
< Net SBC. OK

Minimum pressure below ring wall = $0.22 + 0.16 - 1.45 + 0.01 + 36.28$
= 35.22 kN/m²
No Tension. Hence OK.

CASE IV : DL+OL+0.5LL+SL

Shear force at the base of the tank = 46.54 kN

Total moment on the ringwall at the base of foundation = $0 + 46.53792 \times 2$
= 93.08 kNm

Pressure due to Seismic load M/Zr = $93.08 / 3.95$
= 23.54 kN/m²

P/A = $0.22 + 0.16 + 0.01 \times 0.5 + 36.28$
= 36.67 kN/m²

Maximum pressure below ring wall = $0.22 + 0.16 + 23.54 + 0.01 \times 0.5 + 36.28$
= 60.21 kN/m²
< Hence ok

Minimum pressure below ring wall = $0.22 + 0.16 - 23.54 + 0.01 \times 0.5 + 36.28$
= 13.12 kN/m²
No Tension. Hence OK.

CHECK FOR OVERTURNING

Load case	LOAD COMBINATION	Resisting moment	Overturning moment	Factor of safety	Allowable Factor of safety
1	0.9DL+0.9EL+0.5WL	974.05	2.88	338.80	1.75
2	DL+OL+LL	No overturning moment			1.75
3	DL+OL+LL+WL	1262.50	5.75	219.57	1.75
4	DL+OL+0.5LL+SL	1254.76	93.08	13.48	1.75
5	DL+TL+0.5LL+0.5WL	1254.76	2.88	436.44	1.75

CASE I : (0.9DL+0.9EL+0.5WL)

Empty tank weight = 147.15 kN

Resisting moment due to Empty tank = $0.9 \times 147.15 \times 3.65 / 2$
= 241.69 kNm

$$\begin{aligned}
 \text{Resisting moment due to self weight of ringwall} &= 0.9 * (\pi * 3 * 0.65 * 2 * 30) * 3.65 / 2 \\
 &= 603.73 \text{ kNm} \\
 \text{Resisting moment due to slab} &= ((\pi * 0.25 * 2.35^2) * 0.65 * 25) * 3.65 / 2 \\
 &= 128.63 \text{ kNm} \\
 \text{Total Resisting Moment} \quad \text{RM} &= 241.69 + 603.73 + 128.63 \\
 &= 974.05 \text{ kNm} \\
 \text{Overturning Moment due to Wind} \quad \text{OM} &= 2.88 \text{ kNm} \\
 \text{Factor of safety} = \text{RM} / \text{OM} &= 974.05 / 2.88 \\
 &= 338.80 > 1.75, \text{ Hence OK.}
 \end{aligned}$$

CHECK FOR SLIDING

Load case	LOAD COMBINATION	Resisting Force	Sliding Force	Factor of safety	Allowable Factor of safety
1	0.9DL+0.9EL+0.5WL	266.24	1.92	138.94	1.60
2	DL+OL+LL	No sliding force			1.60
3	DL+OL+LL+WL	333.40	3.83	86.99	1.60
4	DL+OL+0.5LL+SL	333.40	46.54	7.16	1.60
5	DL+TL+0.5LL+0.5WL	333.40	173.99	173.99	1.60

CASE IV : DL+OL+0.5LL+SL

$$\begin{aligned}
 \text{Maximum horizontal force, } F_H &= 46.54 \text{ kN} \\
 \text{Maximum vertical Force} &= W_{OL} + W_{conc} = 245.25 + 70.48 + 306.31 \\
 \text{(Live load is not considered for sliding check)} &= 622.0 \text{ kN} \\
 \text{Co-efficient of friction} &= 0.38 \\
 \text{Sliding Resisting force, } R &= \text{Weight of conc.} * \text{friction} + \text{shear capacity of sand} \\
 &= 622.04 * 0.383 + 95.16 \\
 &= 333.40 \text{ kN} \\
 \text{Factor of Safety against sliding} &= 333.4 / 46.53792 \\
 &= 7.16 > 1.6, \text{ Hence safe}
 \end{aligned}$$

CASE V : DL+TL+0.5LL+0.5WL

$$\begin{aligned}
 \text{Maximum horizontal force, } F_H &= 1.92 \text{ kN} \\
 \text{Maximum vertical Force} &= W_{TL} + W_{conc} = 245.25 + 70.48 + 306.31 \\
 \text{(Live load is not considered for sliding check)} &= 622.0 \text{ kN} \\
 \text{Co-efficient of friction} &= 0.38 \\
 \text{Sliding Resisting force, } R &= \text{Weight of conc.} * \text{friction} + \text{shear capacity of sand} \\
 &= 622.04 * 0.383 + 95.16 \\
 &= 333.40 \text{ kN} \\
 \text{Factor of Safety against sliding} &= 333.4 / 1.91625 \\
 &= 173.99 > 1.6, \text{ Hence safe}
 \end{aligned}$$

DESIGN OF RING WALL

(considering the ring wall is not backfilled)

MATERIAL

Reinforced Concrete

$$\text{Grade of concrete} \quad f_{ck} = 25 \text{ N/mm}^2$$

Steel Reinforcement

$$\text{Grade of steel} \quad f_y = 500 \text{ N/mm}^2$$

Moment due to eccentric loading

$$\begin{aligned}
 \text{Lateral force on ringwall due to fill} &= 0.5 * 19 * (2)^2 / 2 \\
 &= 19.00 \text{ kN/m}
 \end{aligned}$$

$$\begin{aligned}
 \text{Moment due to fill} &= 19 * (2000/2 - 2000/3) / 1000 \\
 &= 6.33 \text{ kNm/m}
 \end{aligned}$$

$$\text{Moment due to load of design fluid on ringwall} = 11.35 * (0.65/2 - 0.321/2)$$

	=	1.87	kNm/m
Moment due to load of test fluid on ringwall	=	$11.56 \cdot (0.65/2 - 0.321/2)$	
	=	1.90	kNm/m
<u>Case I : 1.5DL+1.5EL+0.75WL</u>			
Lateral force on ringwall due to fill	=	$0.5 \cdot 19 \cdot (2)^2 / 2$	
	=	19.00	kN/m
Factored lateral force on ring wall due to fill =	19*1.5	=	28.50 kN/m
Total lateral force	=	28.50	kN/m
Hoop Tension	=	$28.5 \cdot 3/2$	= 42.75 kN
Area of steel required to resist hoop tension	=	Tension / $0.87 \cdot f_y$	
	=	99	mm ²
Total area of steel required to resist hoop tension	=	99	mm ²
<u>Check for Permissible tensile stress</u>			
Unfactored Hoop tension	=	$(19) \cdot 3/2$	
	=	28.50	kN
Actual tensile stress at bottom of wall per unit circumference	=	$F_t / (A_c + m A_{st})$ (Refer IS:456 cl B-2.1.1)	
= $(28.5 \cdot 10^3 / ((650 \cdot 1000 - 99) + (280 / (3 \cdot 8.5)) \cdot 99))$	=	0.04	N/mm ²
Allowable tensile stress (Refer IS:456 cl B-2.1.1 table)	=	3.20	kN/mm ²
			> 0.04 N/mm ² , Hence safe
<u>CASE II : 1.5DL+1.5OL+1.5LL</u>			
Lateral force on ringwall due to operating fluid	=	$0.5 \cdot 10 \cdot 3.537 \cdot 2$	
	=	35.37	kN/m
Factored lateral force on ring wall due to operating fluid	=	53.06	kN/m
Lateral force on ringwall due to Live load	=	$1.2 \cdot 2$	
	=	2.40	kN/m
Factored lateral force on ring wall due to Live load	=	3.60	kN/m
Lateral force on ringwall due to fill	=	$0.5 \cdot 19 \cdot (2)^2 / 2$	
	=	19.00	kN/m
Factored lateral force on ring wall due to fill	=	28.50	kN/m
Total lateral force	=	$53.06 + 3.6 + 28.5$	
	=	85.16	kN/m
Hoop Tension	=	$85.16 \cdot 3/2$	
	=	127.73	kN
Area of steel required to resist hoop tension	=	Tension / $(0.87 \cdot f_y)$	
	=	294	mm ²
Total area of steel required to resist hoop tension	=	294	mm ²
<u>Check for Permissible tensile stress</u>			
Unfactored Hoop tension	=	$(19 + 2.4 + 35.37) \cdot 3/2$	
	=	85.16	kN
Actual tensile stress	=	$(85.16 \cdot 10^3 / ((650 \cdot 1000 - 294) + (280 / (3 \cdot 8.5)) \cdot 294))$	
	=	0.13	N/mm ²
Allowable tensile stress (Refer IS:456 cl B-2.1.1 table)	=	3.20	kN/mm ²
			> 0.13 N/mm ² , Hence safe

Case V : 1.5DL+1.5TL+0.75LL+0.75WL

Lateral force on ringwall due to hydro test fluid = $0.5 \times 10 \times 3.6^2$
 = 36.00 kN/m

Factored lateral force on ring wall due to hydrotest fluid = 36×1.5
 = 54.00 kN/m

Lateral force on ringwall due to fill = $0.5 \times 19 \times (2)^2 / 2$
 = 19.00 kN/m

Factored lateral force on ring wall due to fill = 28.50 kN/m

Total lateral force = $54 + 28.5$ = 82.50 kN/m

Hoop Tension = $82.5 \times 3 / 2$ = 123.75 kN

Area of steel required to resist hoop tension = Tension / $0.87 \times f_y$
 = 285 mm²

Total area of steel required to resist hoop tension and bending = **285** mm²

Check for Permissible tensile stress

Unfactored Hoop tension = $(19 + 36) \times 3 / 2$
 = 82.50 kN

Actual tensile stress = $(82.5 \times 10^3 / ((650 \times 1000 - 285) + (280 / (3 \times 8.5)) \times 285))$ = 0.13 N/mm²

Allowable tensile stress (Refer IS:456 cl B-2.1.1 table) = **3.20** kN/mm²
 > 0.13 N/mm², Hence safe

Horizontal reinforcement for ring wall

Design steel required = 294.00 mm²

Total height of foundation concrete excluding slab Hc = 1350.00 mm

Area of minimum steel required = $0.0020 \times H_c \times w$
 = $0.0020 \times 1350 \times 650$
 = 1755.00 mm²

Area of steel to be provided = 1755.00 mm²

No. of **12** mm dia bars required = 15.52 Nos.
 say **24** numbers

Ast provided = 2714 mm² > 1755 mm²
 Hence safe

Provide 12 numbers on each face.

Spacing of bars provided = 110.36 mm

The maximum spacing is limited to 450 mm & 3*wall thick **Hence safe.**

Vertical reinforcement for ring wall

Area of minimum steel required = $0.0012 \times \text{plan area}$
 = 780 mm² per m

Spacing of **12** mm dia bar = 145 mm c/c.

Provide 12 mm dia bar @ **150** mm c/c.
 Ast provided = 754 mm² < 780 mm²
 Revise

The maximum spacing is limited to 450 mm & 3*wall thick **Hence safe.**

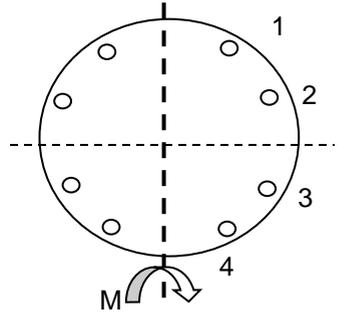
CHECK FOR ANCHOR BOLTS

Cover = **50** mm

Dia of bar = 12 mm

Effective depth = $650 - 50 - 12 / 2$

Dia	=	24	mm
Numbers	=	8	Nos
BCD	=	2500	mm
Projection above rough concrete	=	25+10+150+10+2.5*24	
	=	255	mm
Bolt length	=	43+850+326	
	=	1148.00	mm
Edge distance	=	579.00	mm
Minimum edge distance required	=	142.00	mm
		Hence ok.	
Total shear to be resisted by the bolts	=	46.54	kN
Shear to be resisted by one bolt	=	5.82	kN
Shear capacity of one bolt	=	33.93	kN
		Hence ok.	
Maximum moment occurs due to seismic	=	0.00	kNm
Bolt circle dia	=	5.712	m
Radius	=	2.856	m
Total No of bolts	=	8	
Tension to be carried by	=	4	bolts
Total Shear	=	46.54	kN
Shear per bolt = 46.53792 / 8	=	5.82	kN
Distance of bolt from the axis of Moment for 1,4	=	1.093	m
Distance of bolt from the axis of Moment for 2,3	=	2.639	m
Tension on the Extreme bolt	=	$\frac{M * r}{\sum r^2}$	



$$= \frac{0 * 2.639}{(4 * 1.093^2) + (4 * 2.639^2)}$$

$$= \frac{0.00}{32.64}$$

$$= 0.00 \text{ kN}$$

MS Anchor Bolt

Check for strength of Bolt

Diameter of bolt	=	24	mm
Tensile stress area	=	353.00	mm ² (IS:1367 part3)
Permissible stress in axial tension in bolts	=	120	N/mm ² (IS 800 T-8.1)
Permissible stress in shear in bolts	=	80	N/mm ² (IS 800 T-8.1)
Tension capacity of the section	=	40.00	kN
Shear Capacity of the section	=	25.00	kN
Tension capacity of M24 Bolt =		40.00 kN > 0 kN, Hence safe	

Shear Capacity of M24 Bolt = 25.00 kN > 5.82 kN, Hence safe

CHECK FOR COMBINED SHEAR AND TENSILE STRESS OF BOLTS

Actual shear stress	=	5.82*1000 / 353	
	=	16.49	N/mm ²
Actual tension stress	=	0*1000 / 353	
	=	0.00	N/mm ²
Combined Shear and Tension = $\frac{\text{Actual shear stress}}{\text{Permissible shear stress}} + \frac{\text{Actual tensile stress}}{\text{Permissible tensile stress}}$	=	$\frac{16.49}{80} + \frac{0.00}{120}$	
	=	0.206	<= 1.4

Actual Vs Perm. ratio of Combined Shear and Tensile Stress of bolt is less than 1.4, HENCE SAFE

Seismic Load:

Zone factor	z	=	0.24	
Height of the point of attachment of Equipment	x	=	1.00	m
Height of the building/depth of the foundation	h	=	1.00	m
Importance Factor,	I_p	=	1.50	
Component amplification factor	a_p	=	1	
(Table:11 of IS-1893,Part1 Draft)				
Component Response Modification factor	R_p	=	2.5	
(Table:11 of IS-1893,Part1 Draft)				
Design Horizontal Seismic Coefficient	A_h	=	$Z/2 * (1+(x/h))^* a_p/R_p * I_p$	
Design lateral force on the Equipment	F_p	=	$Z/2 * (1+(x/h))^* a_p/R_p * I_p * W$ $\geq 0.1 * W$	
Design lateral force on the Equipment (as per MDS)	F_{p1}	=	0.00	t
Design lateral force on the Equipment (as per MDS)	F_{p1}	=	0.00	kN
Moment on top of foundation(as per MDS)		=	0.0	t-m
Moment on top of foundation		=	0	kNm
Ext dia of ring wall	D	=	3.65	m
Int dia of ring wall	B	=	2.35	m
Height above ground	h	=	1.00	m
Weight of Block above HPP		=	$B * D * h * 25$	
		=	153.15	kN
Weight of slab 150 thk slab above		=	170.03	kN
Total concrete wt	W_{conc}	=	323.18	kN
Design lateral force on the foundation above FGL	F_{p2}	=	$0.24/2*(1+1/1)*1/2.5*1.5*323.18$	
	F_{p2}	=	46.54	kN
Total shear on top of foundation		=	46.54	kN

Wind Data:

Basic wind speed / velocity	V _b	=	50.0	m/s
	k ₁	=	1.00	(Table 1 IS 875 Part 3)
	k ₂	=	1.00	(Table 2 IS 875 Part 3)
	k ₃	=	1.00	
Design Wind Speed $V_z = V_b * k_1 * k_2 * k_3$		=	50.00	m/s
Design Wind Pressure $P_z = 0.6 V_z^2$		=	1500.00	N/m ²
	P_z	=	1.50	kN/m ²
External dia of tank		=	3.02	m
External dia of RING WALL		=	3.65	m
Height of ring wall above FGL		=	1.00	m
Total ht of ring wall		=	2.00	m
Wall height / breadth ratio of tank		=	3.6 / 3.016	
		=	1.19	
C(f)		=	0.70	(Table 24 for b/h ratio 1 to 12)
F		=	P _z * C(f) * D _e * H	
		=	1.5 * 0.7 * 3.016 * 3.6	
Wind shear (As per MDS)	F₁	=	0.00	t
Wind shear (As per MDS)	F₁	=	0.00	kN
Moment at the bottom of foundation "M1"		=	0.00	t-m
Moment at the bottom of foundation "M1"		=	0.00	kNm
Moment at the bottom of foundation "M2"		=		
Due to shear at top of ring beam		=	0	kNm
Wind shear on ring wall	F₂	=	3.83	kN
Moment at the bottom of foundation "M3"		=	5.75	kNm
Total shear		=	3.83	kN
Total moment at the bottom of foundation		=	5.75	kNm