

DESIGN OF GROUND FLOOR SLAB (TWO WAY SLAB)**Condition : Interior Panels****DESIGN DATA:-**

Span of slab in shorter direction	l_a	=	3274	mm	3.274 m	
Span of slab in longer direction	l_b	=	4150	mm	4.150 m	
Thickness of Slab Provided	h_p	=	150	mm	0.150 m	
Clear cover to main reinf.	d'	=	30	mm		
Dia of main reinforcement	ϕ	=	12	mm	(Shorter span)	
Dia of main reinforcement	ϕ	=	12	mm	(Long span)	
Eff. depth of slab (Short span)	d_{sa}	=	(150 - 30 - 6)	=	114 mm	Shorter span
Eff. depth of slab (Long span)	d_{sb}	=	(150-12-30-6)	=	102 mm	Long span
Density of Concrete	γ_c	=	25	kN/m ³		
Compressive strength of concrete	f_c'	=	35	N/mm ²		Ref.Design Basis
Yield Strength of steel	f_y	=	420	N/mm ²		

LOADINGS

Dead load	Considering the width of slab as	b	=	1000 mm	
Self weight of slab	=	0.15×25	=	3.750 kN/m ²	
Dead load due to electrical accessories	=	1.000 kN/m ²			
Total Dead load	DL	=	4.75	kN/m ²	
Factored dead load	W_{ud}	=	$1.2 \times DL$	=	5.70 kN/m ²
	LL	=	9.00	kN/m ²	Ref.Design Basis
	W_{ul}	=	$1.6 \times LL$	=	14.40 kN/m ²
Total Factored load	RLL	=	5.7 + 14.4		
		=	20.100	kN/m ²	

DESIGN

The slab is designed using moment coefficients method.

Ratio of shorter / longer span = $3.274 / 4.15 = 0.79$ Two way slab

Edge conditions of the slab

Case 1

Moments in shorter direction $M_a = C_a \times W \times l_a^2$

Moments in longer direction $M_b = C_a \times W \times l_b^2$

W = Uniform load on the slab ; l_a & l_b are span in short and long directions respectively

Negative moments $M (-ve) = C_a \times W_u \times l^2$ Continuous Edge

Moments due to Dead Load $M (+ve) = C_{ad} \times W_{ud} \times l^2$ Mid spans

Moments due to Live Load $M (+ve) = C_{al} \times W_{ul} \times l^2$ Mid spans

Negative moments for Short span = $1/3 \times +ve$ Moments Discontinuous Edge

Moments coefficients (-ve)	$C_a (-ve)$	=	0.0000	$C_b (-ve)$	=	0.0000
Moments coefficients (+ve) DL	$C_{ad} (+ve)$	=	0.0571	$C_{bd} (+ve)$	=	0.0221
Moments coefficients (+ve) LL	$C_{al} (+ve)$	=	0.0571	$C_{bl} (+ve)$	=	0.0221

Negative moments (Short Span) $M_a (-ve) = 0 \times 20.1 \times 3.274^2 = 0.00$ kN-m Continuous Edge

Negative moments (Long Span) $M_b (-ve) = 0 \times 20.1 \times 4.15^2 = 0.00$ kN-m Continuous Edge

Positive moments (short Span) $M_{ad} (+ve) = 0.0571 \times 5.7 \times 3.274^2 = 3.49$ kN-m Due to dead load

Positive moments (short Span) $M_{al} (+ve) = 0.0571 \times 14.4 \times 3.274^2 = 8.8136531$ kN-m Due to Live load

Total +ve moments (short Span) $M_a (+ve) = 12.30$ kN-m

Positive moments (Long Span) $M_{bd} (+ve) = 0.0221 \times 5.7 \times 4.15^2 = 2.170$ kN-m Due to dead load

Positive moments (Long Span) $M_{bl} (+ve) = 0.0221 \times 14.4 \times 4.15^2$ Due to Live load

Total +ve moments (Long Span) $M_b (+ve) = 5.481$ kN-m
 $= 7.650$ kN-m Discontinuous edges

Negative moments for Short span $= 1/3 \times 12.302$
 $= 4.101$ kN-m

Negative moments for Long span $= 1/3 \times 7.65$ Discontinuous edges
 $= 2.6$ kN-m

Main reinforcement (Shorter & Longer Span)

Moment Factor $R_u = \frac{M_u / \phi \times b \times d^2}{1000 \times (1 - \sqrt{1 - (2R_u \times 1000 / fy)})}$ $\phi = 0.9$
 Percentage of steel required $\rho = \frac{m}{fy / 0.85 \times fc'}$ $= 14.118$
 But Minimum percentage of steel $\rho_{min} = 0.18\%$

CI 7.12.2.1.C
 ACI 318-14

Design of Reinforcement for Shorter Span :-

Factored Moment	Moment kN-m	Factor R_u	Reqd% of steel	Provided % of steel	Area of steel	C/C Spacing of 12 mm Dia bar
Continuous edges	0.000	0.000	0.0000	0.0018	205.200	550 mm c/c
Mid Span	12.302	1.052	0.0026	0.0026	290.715	375 mm c/c
Discontinuous edges	4.101	0.351	0.0008	0.0018	205.200	550 mm c/c

Reinforcement steel Provided = 12 mm Dia bar 200 mm c/c For Short Span

Design of Reinforcement for Long Span :-

Factored Moment	Moment kN-m	Factor R_u	Reqd% of steel	Provided % of steel	Area of steel	C/C Spacing of 12 mm Dia bar
Continuous edges	0.000	0.000	0.0000	0.0018	205.200	550 mm c/c
Mid Span	7.650	0.654	0.0016	0.0018	205.200	550 mm c/c
Discontinuous edges	2.550	0.218	0.0005	0.0018	205.200	550 mm c/c

Reinforcement steel Provided = 12 mm Dia bar 200 mm c/c For long Span

Shrinkage and Temperature Reinforcement

Effective Area of concrete $= b \times D = 150000$ mm²
 Minimum percentage of steel $= 0.18\%$
 Area of steel required $A_{st} = 270$ mm² (For Both ways)
 Assuming dia of bar $dbt = 10$
 Spacing of 10 mm dia bar $= 582$ mm (For Single face)
 Provide 10 dia bars @ 200 mm C/C

CI 7.12.2.1.C
 ACI 318-14

Check for Shear :-

Factored Shear Force $Q_u = 20.1 \times 4.15/2 = 41.7$ kN
 Allowable shear force by concrete $\phi V_c = 0.75 \times [(1/6) \times \sqrt{fc'} \times b \times dsb]$
 $\phi V_c = 75.4$ kN > 41.71

Factored shear force is less than allowable shear force provided by concrete. So safe.

Required Thickness of Slab

Min thickness of Slab require $= \frac{l_n \times (0.8 + (fy / 1400))}{36 + (9\gamma)}$
 $l_n =$ Clean Span on Longer side $= 4150$ mm
 $\gamma = l_b / l_s = (300 \times 500^3 / 12) / (1000 \times 200^3 / 12) = 4.6875$
 $\gamma = \frac{4150}{3274} = 1.2676$
 Min thickness of Slab require $= 4150 \times (0.8 + (420/1400))$

$$= \frac{36+(9 \times 1.268)}{1000} = 96.292 \text{ mm approx } 90 \text{ mm}$$

$$< 200 \text{ mm Provided slab thickness}$$

Deflection Due to Loads:

$$\text{Allowable deflection} = \frac{\text{Span}}{360} = \frac{4150}{360} = 11.528 \text{ mm As per Table 24.2.2, ACI 318 - 19}$$

$$\text{Actual deflection in slab due to loads} = \frac{K w l^4}{384 E I}$$

- K = deflection coefficient depending on support condition = 2
- w = Loads acting on slab (Dead load + Live load) = 13.75 kN/m²
- L = Span = 4150 mm
- E = $W_c^{1.5} \times 0.043 \text{ sqrt}(f_c)$ = 26229 kN/m³ As per cls. 19.2.2.1, ACI 318-19
- = $2380^{1.5} \times 0.043 \times \text{sqrt}(27.6)$
- I = $(1000 \times 200^3) / 12$ = 7E+08 mm⁴

$$\text{Actual deflection in slab due to loads} = \frac{2 \times 13.75 \times 4150^4}{384 \times 26229.405 \times 666666666.67}$$

$$= 1.215 \text{ mm}$$

$$< 11.528 \text{ mm}$$

Hence Safe