

## CHECK FOR ANCHOR BOLTS:

### 1 Strength of Anchor Bolt under tension(Pulling force)

Strength reduction factor ( $\phi$ )	=	0.7	ACI 318-14 – 17.3.3
Tensile Area of Bolt	=	$0.7854 \cdot (28 - (0.9743/40))^2$	489.92 mm <sup>2</sup>
Fu	=	420 N/mm <sup>2</sup>	
Pullout strength = $\phi \times A_t \times f_u$	=	$0.7 \times 489.919 \times 420 / 1000$	= 144.0362 kN
Tension Force from structure	=		= 93.831 kN <b>Hence Safe</b>

$$A_t = 0.7854 \cdot [d - (0.9743 / n)]^2,$$

### Steel strength of anchor in tension

Steel strength of anchor in tension is determined according to ACI 318-14 – 17.4.1 as

$$\phi N_{sa} = \phi A_{se,N} f_{uta}$$

where:

- $\phi = 0.7$  - strength reduction factor for anchors in tension according to ACI 318-14 – 17.3.3, the factor is editable in Code setup
- $A_{se,N}$  - tensile stress area
- $f_{uta}$  - specified tensile strength of anchor steel and shall not be greater than  $1.9 f_{ya}$  and 125 ksi

Concrete pullout strength of an anchor is defined in ACI 318-14 – 17.4.3 as

$$\phi N_{pn} = \phi \psi_{c,p} N_p$$

where:

- $\phi = 0.7$  - strength reduction factor for anchors in tension according to ACI 318-14 – 17.3.3, editable in Code setup
- $\psi_{c,p}$  - modification factor for concrete condition;  $\psi_{c,p} = 1.0$  for cracked concrete,  $\psi_{c,p} = 1.4$  for non-cracked concrete
- $N_p = 8 A_{brg} f'_c$  for headed anchor
- $A_{brg}$  - bearing area of the head of stud or anchor bolt
- $f'_c$  - concrete compressive strength

Concrete pullout strength for other types of anchors than headed is not evaluated in the software and has to be specified by the manufacturer.

### 2 Check for Concrete Pullout Strength

Strength reduction factor ( $\phi$ )	=	0.7	ACI 318-14 – 17.4.3
Modification Factor ( $\psi$ )	=	1.0	
Pullout strength = $8 \times A_{br} \times f'_c$	=	$8 \cdot ((\pi)/4) \cdot 25^2 \cdot 30$	= 147.7805 kN
Tension Force from structure	=		= 93.831 kN <b>Hence Safe</b>

### 3 Embedment Length

Minimum embedment length for lug	=	$12d \sqrt{\frac{F_u}{58\psi}}$	
Dia of Anchor Bolt provided	=	25 mm	
Required embedment length for lug	=	$12 \cdot 25 \cdot \text{SQRT}((30 \cdot 0.9) / 58 \cdot 0.5)$	
	=	145 mm	
Provided embedment length for lug	=	500 mm	
		<b>Hence Safe</b>	

### 4 Check for Concrete Break out test:

Provided embedment depth	=	500 mm	
Embedment Length	=	$1.5 \times h_{ef} =$	750 mm
$A_{Nco} = 9 h_{ef}^2$	=	5062500	mm <sup>2</sup>
$A_{Nc} = A = \pi r l + \pi r^2$	=	1180000	mm <sup>2</sup>
$k_c$	=	16	
$f'_c$	=	30 N/mm <sup>2</sup>	
$\lambda_a$	=	0.65	
$h_{ef}$	=	500 mm	

$$N_b = 16 \lambda_a \sqrt{f'_c} h_{ef}^{5/3} = 1185.6 \text{ kN}$$
$$= 93.8 \text{ kN} \quad \text{Hence Safe}$$

$$N_b = k_c \lambda_a \sqrt{f'_c} h_{ef}^{1.5}$$

**Group Anchor Bolt check for Tension:**

Base Plate size = L = 250 mm B = 250 mm  
 Angle on Base plate = 65 x 65 x 8 mm  
 Thickness of Base Plate = t = 20 mm  
 Dia of Achor Bolt = 25 mm  
 Dia of Bolt Hole = 28 mm  
 Base plate Edge distance to centre of bolt hole = 50 mm  
 Distance c/c of Bolt = 150 mm  
 Diagonal distance c/c of Bolt = 212 mm  
 CG of Plate for top view = 125 mm  
 No of Bolts = 4 nos  
 Max.Tension in the support structure = 93.8 kN  
 Tension taken per bolt = 23.5 kN  
 Effective Embedment Depth ( $h_{ef}$ ) = 300  $\approx$  350 mm (As per PIP STE05121. Table-1)  
 Max.c/c distance between the Bolts ( $s_1$ ) = 212 mm  
 Offset of concrete from base plate = 125 mm  
 Distance b/w centre of bolt to concrete edge ( $C_{a1}$ ) = 175 mm  
 $1.5 \times h_{ef} = 525$  mm

**Check for  $C_{a1}$  &  $s_1$ :**

a)  $C_{a1} < 1.5 \times h_{ef} = 175 \text{ mm} < 525 \text{ mm}$  **SAFE**  
 b)  $s_1 < 3.0 \times h_{ef} = 212 \text{ mm} < 1050 \text{ mm}$  **SAFE**

**Calculation of  $A_{Nc}$  Projected concrete failure area of group anchors**

$$A_{Nc} = (C_{a1} + s_1 + 1.5h_{ef}) \times (2 \times 1.5h_{ef})$$

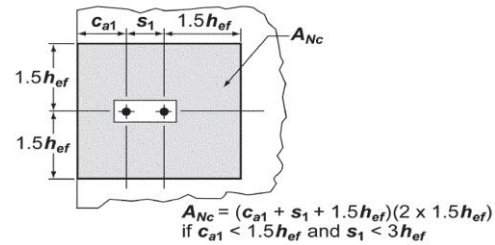
$$= (175+212+525) \times (2 \times 525)$$

$$= 957738.6 \text{ mm}^2$$

$$A_{Nco} = 9.0 \times h_{ef}^2$$

$$= 9.0 \times 525 \times 525$$

$$= 2480625.0 \text{ mm}^2$$



**Check**

$A_{Nc}$  shall not exceed  $nA_{Nco}$  Cl.17.4.2.1 (ACI-318-14)

$$n A_{Nco} = 2 \times 2480625 \quad n = 4$$

$$4961250 \text{ mm}^2$$

$A_{Nc} < A_{Nco}$  **SAFE**

**Check**

$h_{ef}$  Shall be more than 11 inches and less than 25 inches Cl.17.4.2.2 (ACI 318-14)

11 inch < 13.78 inch < 25 inch  
 279 mm < 350 mm < 635 mm **SAFE**

**The basic concrete breakout strength in tension in cracked concrete,  $N_b$**

$$N_b = k_c \lambda_a \sqrt{f'_c} h_{ef}^{1.5} = 24 \times 1 \times \text{SQRT}(27.5) \times 350^{1.5} \text{ Cl.17.4.2.2 (ACI-318-14)}$$

$k_c = 24 = 824.10 \text{ kN}$   
 $\lambda_a = 1.0$   
 $f'_c = 27.5 \text{ N/mm}^2$   
 $h_{ef} = 350 \text{ mm}$

**The nominal concrete breakout strength in tension,  $N_{cbg}$  of a group of anchors**

$$N_{cbg} = \frac{A_{Nc}}{A_{Nco}} \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$$

ACI 318-14 Cl.17.4.2.1

$\Psi_{ec,N} = 1$  Eccentricity = 0 mm  $\Psi_{c,N} = 1.25$   
 $1/1+((2*0)/(3*350))$

$\Psi_{ed,N} = 0.8$   $\Psi_{cp,N} = 0.9$   
 $C_{a1} < 1.5 \times h_{ef}$   
 $175 \text{ mm} < 525 \text{ mm}$   
 $0.7+(0.3*(175/525))$

$A_{Nc} = 957738.6 \text{ mm}^2$   
 $A_{Nco} = 2480625.0 \text{ mm}^2$   
 $N_b = 824.1 \text{ kN}$   
 $N_{cbg} = 286.357166 \text{ kN}$

### Steel Strength of Anchor in Shear :

$$A_{seV} = A_{se,V} = \frac{\pi}{4} \left( d_a - \frac{0.9743}{n_t} \right)^2 = 489 \text{ mm}^2$$

$$f_{uta} = 500 \text{ N/mm}^2$$

$$V_{sa} = V_{sa} = 0.6 A_{se,V} f_{uta} = 245 \text{ kN} \quad \text{SAFE}$$

$$N_{sa} = A_{se,V} f_{uta} \quad (17.4.1.2)$$

### Group Anchor Bolt check for Shear:

Projected concrete failure area of group of anchors  $A_{Vc}$

$$A_{Vc} = 2(1.5 c_{a1}) h_a = 2 * (1.5 * 175) * 20 = 10500 \text{ mm}^2$$

$$C_{a1} = 175 \text{ mm}$$

$$h_a = 20 \text{ mm}$$

$$A_{Vco} = 2(1.5 c_{a1}) \times (1.5 c_{a1}) = 4.5 c_{a1}^2$$

$$C_{a1} = 175 \text{ mm} = 4.5 * 175^2 = 1E+05 \text{ mm}^2$$

### Check $\ell_e \leq 8d_a$

$$8.0 \times d_a = 200 \text{ mm}$$

$$h_{ef} = 350 \text{ mm}$$

$$\ell_e = \min \text{ of } 8.0 \times d_a \text{ \& \ } h_{ef} = \text{MIN}(200, 350) = 200 \text{ mm}$$

$$V_b = \left( 7 \left( \frac{\ell_e}{d_a} \right)^{0.2} \sqrt{d_a} \right) \lambda_a \sqrt{f_c'} (c_{a1})^{1.5}$$
$$V_b = \frac{7 * ((200/25)^{0.2}) * (25^{0.5}) * 1 * (30^{0.5}) * (175^{0.5})}{1000} = 3.84 \text{ kN}$$

$$\Psi_{ec,V} = 1 \quad \text{Eccentricity} = 0 \text{ mm}$$

$$\Psi_{ed,V} = 1.0 \quad 0.7 + (0.3 * (262.5 / (1.5 * 175)))$$
$$C_{a1} = 175 \text{ mm} \quad C_{a2} = 262.5 \text{ mm}$$

$$\Psi_{c,V} = 1.4$$

$$\Psi_{h,V} = 3.6$$

$$V_{cbg} = \frac{A_{Vc}}{A_{Vco}} \Psi_{ec,V} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} V_b \quad (17.5.2.1b) = \frac{10500}{137812.5} * 1 * 1 * 1.4 * 3.6 * 3.8 = 1.4854 \text{ kN}$$

$$A_{seV} = A_{se,V} = \frac{\pi}{4} \left( d_a - \frac{0.9743}{n_t} \right)^2 = \frac{(\pi/4) * (25 - 0.9743/25)^2}{1} = 489 \text{ mm}^2$$

$$f_{uta} = 500 \text{ N/mm}^2$$

$$V_{sa} = A_{se,V} f_{uta} = 244.7 \text{ kN} \quad \text{SAFE}$$

Table 1 - Minimum Anchor Dimensions – U.S. Customary Units

(See Figure 1 for dimension locations)

ANCHOR ROD DIAMETER	EFFECTIVE CROSS-SECTIONAL AREA OF ANCHOR ROD IN TENSION (Note 3)	HEAVY HEX HEAD/NUT WIDTH	ANCHOR TYPE 2 THREAD LENGTH AT BOTTOM OF ANCHOR		ASCE ANCHORAGE DESIGN REPORT MINIMUM DIMENSIONS (Note 1)				SLEEVES (See Note 1 (d))		
					$h_{ef}$	EDGE DISTANCE $c_a$ (Note 2)		SPACING			
			$d_a$	$A_{se,N}$	$W_h$	WITH NO AP	WITH AP (Note 4)	$12d_a$	A307/A36 F1554 GRADE 36	HIGH-STRENGTH (> 36 ksi) OR TORQUED ANCHORS	$4d_a$
			TB1	TB2		$4d_a \geq 4.5"$	$6d_a \geq 4.5"$		Diam $d_s$	Height $h_s$	$6d_a \geq 6"$
in.	in <sup>2</sup>	in.	in.	in.	in.	in.	in.	in.	in.	in.	in.
5/8	0.226	1.25	1.25	–	7.5	4.5	4.5	2.5	2	7	6
3/4	0.334	1.44	1.25	2.25	9.0	4.5	4.5	3.0	2	7	6
7/8	0.462	1.69	1.50	2.50	10.5	4.5	5.3	3.5	2	7	6
1	0.606	1.88	1.75	3.00	12.0	4.5	6.0	4.0	3	10	6
1-1/4	0.969	2.31	2.00	3.50	15.0	5.0	7.5	5.0	–	–	–
1-1/2	1.405	2.75	2.25	4.00	18.0	6.0	9.0	6.0	–	–	–
1-3/4	1.900	3.19	2.50	4.75	21.0	7.0	10.5	7.0	–	–	–
2	2.500	3.63	2.75	5.25	24.0	8.0	12.0	8.0	–	–	–
2-1/4	3.250	4.06	3.00	5.75	27.0	9.0	13.5	9.0	–	–	–
2-1/2	4.000	4.50	3.50	6.50	30.0	10.0	15.0	10.0	–	–	–
2-3/4	4.930	4.94	3.75	7.00	33.0	11.0	16.5	11.0	–	–	–
3	5.970	5.31	4.00	7.75	36.0	12.0	18.0	12.0	–	–	–

$$A_{Nco} = (2 \times 1.5h_{ef}) \times (2 \times 1.5h_{ef}) = 9h_{ef}^2$$

(b) For a group of anchors

$$N_{cbg} = \frac{A_{Nc}}{A_{Nco}} \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \quad (17.4.2.1b)$$

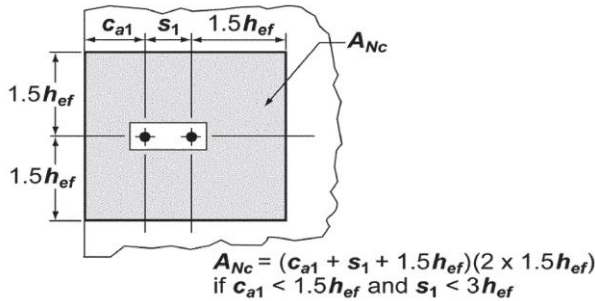
$$\psi_{ec,N} = \frac{1}{1 + \frac{2e'_N}{3h_{ef}}}$$

If  $c_{a,min} \geq 1.5h_{ef}$ , then  $\psi_{ed,N} = 1.0$

If  $c_{a,min} < 1.5h_{ef}$ , then  $\psi_{ed,N} = 0.7 + 0.3 \frac{c_{a,min}}{1.5h_{ef}}$

(a)  $\psi_{c,N} = 1.25$  for cast-in anchors

(b)  $\psi_{c,N} = 1.4$  for post-installed anchors, where the value of  $k_c$  used in Eq. (17.4.2.2a) is 17



If  $c_{a,min} \geq c_{ac}$ , then  $\psi_{cp,N} = 1.0$

If  $c_{a,min} < c_{ac}$ , then  $\psi_{cp,N} = \frac{c_{a,min}}{c_{ac}}$

### 17.5.2 Concrete breakout strength of anchor in shear

17.5.2.1 The nominal concrete breakout strength in shear,  $V_{cb}$  of a single anchor or  $V_{cbg}$  of a group of anchors, shall not exceed:

(a) For shear force perpendicular to the edge on a single anchor

$$V_{cb} = \frac{A_{vc}}{A_{vco}} \psi_{ed,V} \psi_{c,V} \psi_{h,V} V_b \quad (17.5.2.1a)$$

(b) For shear force perpendicular to the edge on a group of anchors

$$V_{cbg} = \frac{A_{vc}}{A_{vco}} \psi_{ec,V} \psi_{ed,V} \psi_{c,V} \psi_{h,V} V_b \quad (17.5.2.1b)$$

$$(a) V_b = \left( 7 \left( \frac{\ell_a}{d_a} \right)^{0.2} \sqrt{d_a} \right) \lambda_a \sqrt{f'_c} (c_{a1})^{1.5} \quad (17.5.2.2a)$$

$$V_{cbg} = \frac{A_{vc}}{A_{vco}} \Psi_{ec,V} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} V_b \quad (17.5.2.1b)$$

$$A_{vco} = 4.5(c_{a1})^2 \quad (17.5.2.1c)$$

$$A_{vc} = 2(1.5c_{a1})h_a$$

$$\Psi_{ed,V} = 0.7 + 0.3 \frac{c_{a2}}{1.5c_{a1}}$$

$$\Psi_{ec,Na} = \frac{1}{\left(1 + \frac{e'_N}{c_{Na}}\right)}$$

$$\Psi_{c,V} = 1.4$$

$$\Psi_{h,V} = \sqrt{\frac{1.5c_{a1}}{h_a}} \quad (17.5.2.8)$$

$$V_{sa} = A_{se,V} f_{uta} \quad (17.5.1.2a)$$

$$A_{se,V} = \frac{\pi}{4} \left( d_a - \frac{0.9743}{n_t} \right)^2$$